









# Labyrinth Spillways in USA

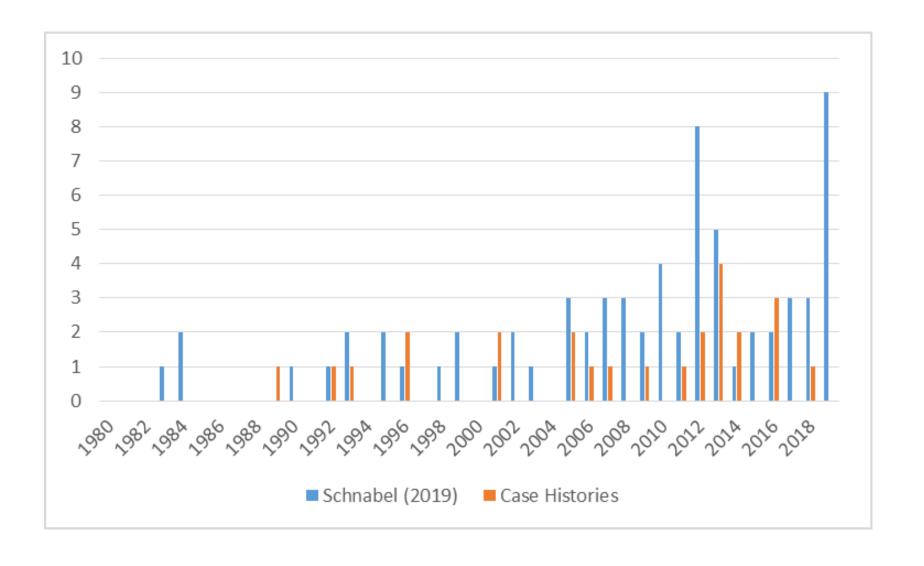








## Labyrinth Spillways in USA



#### BALANCING SITE CONSIDERATIONS WITH HYDRAULIC EFFICIENCY FOR LABYRINTH SPILLWAYS

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Dave Campbell, P.E.<sup>4</sup>

#### ABSTRACT

Labyrinth spillways are relatively common in the rehabilitation of dams that do not meet spillway design flood requirements. While hydraulically efficient (high discharge per unit width of spillway for a given head) designs are desirable, hydraulic optimization is not always prudent due to increased construction costs and site constraints. As designers, we acknowledge and accept a diminished hydraulic efficiency when the reduction is balanced against construction costs.

This paper presents a review of key geometric parameters related to the design of labyrinth weirs and describes how each parameter can impact construction cost and hydraulic performance. Several labyrinth spillway projects are highlighted to illustrate the influence of site conditions on the design.

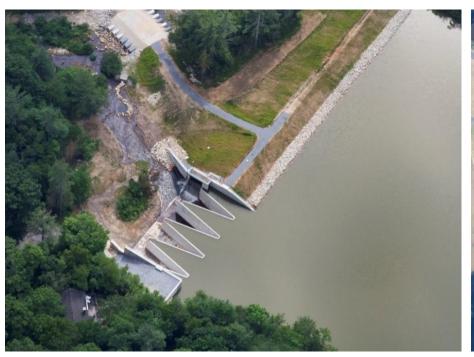
While labyrinth spillways are hydraulically most efficient at low headwater ratios (H/P), it is common practice in design for the maximum H/P to be greater than 0.7 but less than 1.0, which approximates the limit of historic physical model data sets used in readily available publications. The results of recent hydraulic modeling have revealed that weirs with H/P ratios well above 1.0 can be used without significant incremental loss of hydraulic efficiency. Constructability and cost evaluations are also presented with regard to the impacts of nappe interference and disturbance length limits suggested by Falvey (2003). Applying these restrictions can lead to larger upstream-downstream dimensional requirements and larger sidewall angles. Similar cost evaluations are performed to consider cycle width (W/P) ratios lower than recommended by common design methods. While not as hydraulically efficient, high head labyrinths and compact plan-form labyrinths can meet hydraulic design criteria in many site settings at lower overall cost.

# Common Applications





# Common Applications





ID Project Name	State	n	P (ft)	nxW (ft)	α	W/P	Max H/P
1 Roy F. Varner Reservoir Dam	GA	8	10	160	13.9	2.0	0.70
2 Dog River - original	GA	8	15	240	13.0	2.0	0.60
3 Lake Sovereign Dam	GA	2	5	50	12.6	5.0	0.80
4 Concourse Lake Dam	VA	2	10.9	24	10.5	1.1	0.32
5 Accord Pond Dam	MA	2	1.7	7	12.5	2.1	0.88
6 Hollis G Lathem Reservoir Dam	GA	3	15	90	12.6	2.0	0.53
7 Unicoi State Park Dam	GA	3	16	115	10.3	2.4	0.94
8 Whitewater Creek Dam	GA	12	13	360	13.3	2.3	0.31
9 Yahoola Creek Dam	GA	5	15	130	8.9	1.7	0.87
10 DRA Detention Structure <sup>1</sup>	GA	4	13.5	81	16.7	1.5	0.30
10 DRA Detention Structure <sup>2</sup>	GA	4	15.5	81	16.7	1.3	0.13
11 Waterford Lake Dam	NC	3	10	60	8.6	2.0	0.50
12 Lake Upchurch Dam	NC	6	12	120	8.6	1.7	0.42
13 Capital City Country Club Dam	GA	1	10.2	23	23.8	2.3	0.78
14 Pine Lake Dam	GA	2	7.5	30	6	2.0	0.53
15 Pye Lake Dam	GA	3	13	36	7.0	0.9	0.08
16 Dog River – raised	GA	8	25	240	12.2	1.2	0.36
17 Huntington Hills Dam	SC	3	12.5	78	9.7	2.1	0.15
18 Linville Land Harbor Dam <sup>3</sup>	NC	4	15	120	12.2	2.0	0.60
18 Linville Land Harbor Dam <sup>3</sup>	NC	4	19	120	12.2	1.6	0.47
19 Pine Run Dam <sup>1</sup>	PA	0.5	6	11	9.1	3.7	0.75
19 Pine Run Dam <sup>2</sup>	PA	3.5	7.9	77	9.1	2.8	0.33
20 Lake Townsend Dam <sup>1</sup>	NC	2	20	84	12.8	2.1	0.75
20 Lake Townsend Dam <sup>2</sup>	NC	5	21	210	12.8	2.0	0.67
21 Leaser Lake Dam <sup>1</sup>	PA	0.5	12	12.5	14.0	2.1	0.67
21 Leaser Lake Dam <sup>2</sup>	PA	1.5	13.5	37.5	12.3	1.9	0.79
22 Greystone Development Dam	GA	1	8	35	8.7	4.4	0.59
23 Indian Run Dam <sup>1</sup>	PA	0.5	9	16	10.9	3.6	0.89
23 Indian Run Dam <sup>2</sup>	PA	2	11.5	64	10.9	2.8	0.48
24 Upper Norton Dam	VA	3	10.5	63	12.1	2.0	0.43
25 Upper Owl Creek Dam <sup>1</sup>	PA	0.5	8.5	9 75	10 1	23	0 94

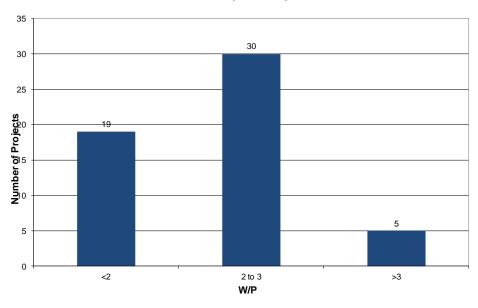
ID	Project Name	State	n	P (ft)	nxW (ft)	α	W/P	Max H/P
25	Upper Owl Creek Dam <sup>1</sup>	PA	0.5	8.5	9.75	10.1	2.3	0.94
25	Upper Owl Creek Dam <sup>2</sup>	PA	2.5	11	48.75	10.1	1.8	0.50
26	Lake Natalie Dam	GA	4	10.5	84	9.8	2.0	0.76
27	Charter Colony, LTC 20/25 <sup>1</sup>	VA	0.3	10.7	3.54	7.0	1.1	0.36
27	Charter Colony, LTC 20/25 <sup>2</sup>	VA	1.7	13.5	20.06	6.2	0.9	0.07
28	Kauffman Dam <sup>1</sup>	PA	0.5	5.5	9	8.6	3.3	0.91
28	Kauffman Dam²	PA	4.5	8	81	8.0	2.3	0.31
29	South River No. 29	GA	3	13	78	10.5	2.0	0.77
30	Tired Creek Dam	GA	3	13	78	9.0	2.0	0.72
31	Beaver Creek Dam	PA	30	6.25	300	10.1	1.6	0.96
32	Charter Colony, LTC 30	VA	4	12	72	8.8	1.5	0.28
33	Charter Colony, LTC 5	VA	2	12	37	8.2	1.5	0.23
34	Dees Pond Dam	GA	2	12	56	19.2	2.3	0.40
35	Ford Road Dam	GA	1	17.75	14	18.2	0.8	0.34
36	Hard Labor Creek Dam	GA	4	15	128	7.9	2.1	0.80
37	Lake Carroll Dam	GA	4	12	86	10.6	1.8	0.50
38	Long Island Drive	GA	1	12.75	13	18.4	1.0	0.47
39	Minsi Lake Dam <sup>1</sup>	PA	5	10	125	11.4	2.5	0.75
39	Minsi Lake Dam <sup>2</sup>	PA	5	12.5	125	11.8	2.0	0.44
40	Mountain Cove Dam	GA	1	8	22	7.7	2.8	0.63
41	Pilot Mountain State Park Dam	NC	2	8	17.5	8.8	1.1	0.50
42	South River No. 4	GA	2	13.5	54	10.3	2.0	0.78
43	Upper Dam	ME	4	14	112	10.4	2.0	0.28
44	Yellow River No. 3	GA	2	13	62	7.7	2.4	0.27

For each of the projects listed in Table 1, various alternative geometric layouts were evaluated for the authors. These figures summarize different geometric parameters selected for the projects in Table 1.

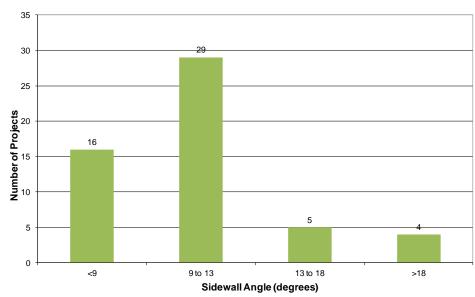
Through these designs, the authors have found the following general trends:

- ◆ Decreasing the sidewall angle typically reduces the total project cost.
- ♦ While lower W/P values generally result in less efficient hydraulic designs, lower W/P values have been found to result in more economical labyrinth spillways.
- ♦ For most projects, the designers have maximized the H/P ratio within the range of the design guidance.

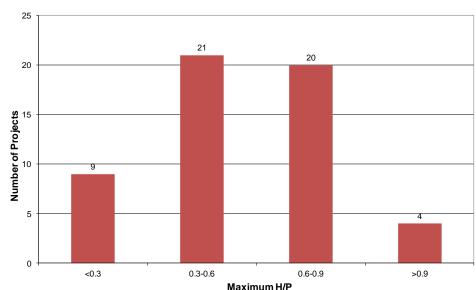
#### W/P Values for Labyrinth Projects in Table 1



#### Sidewall Angle for Labyrinth Projects in Table 1



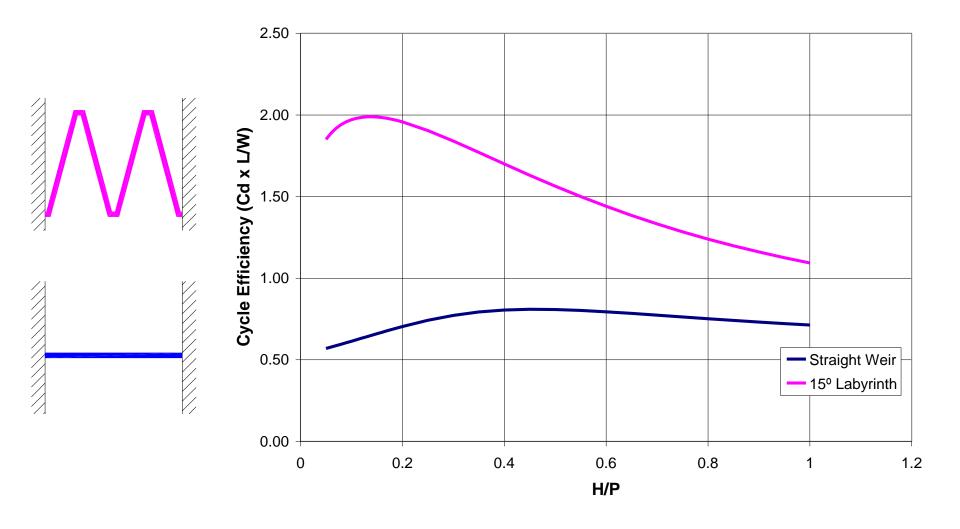
#### Maximum H/P for Labyrinth Projects in Table 1



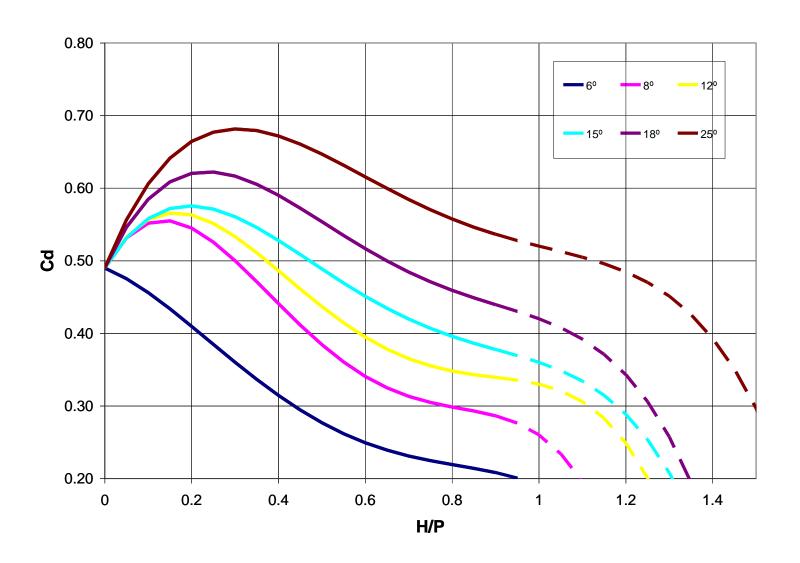
# Large H/P Values



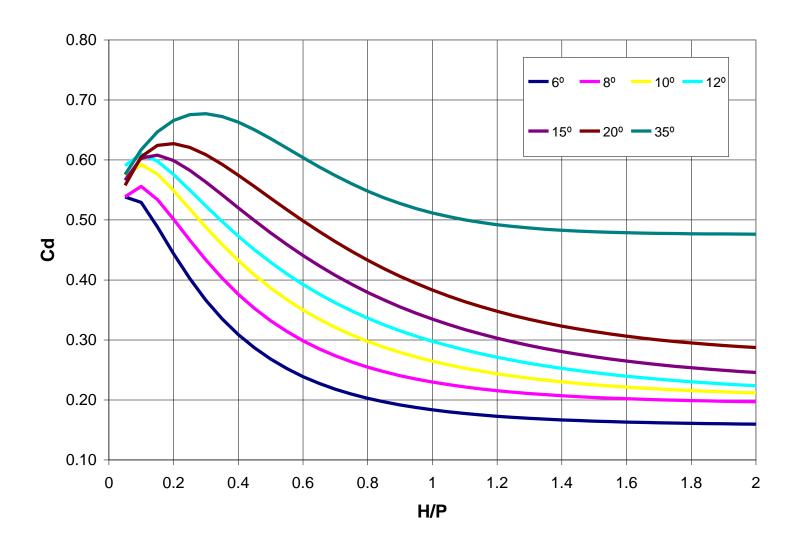
## Purpose of Study



## Tullis et al (1995): Polynomial Equations



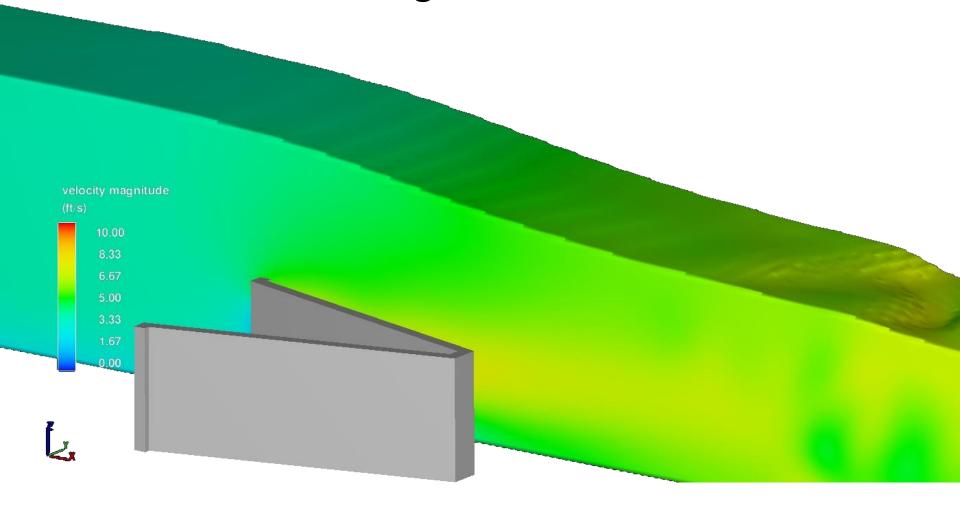
## Crookston (2010) Equations



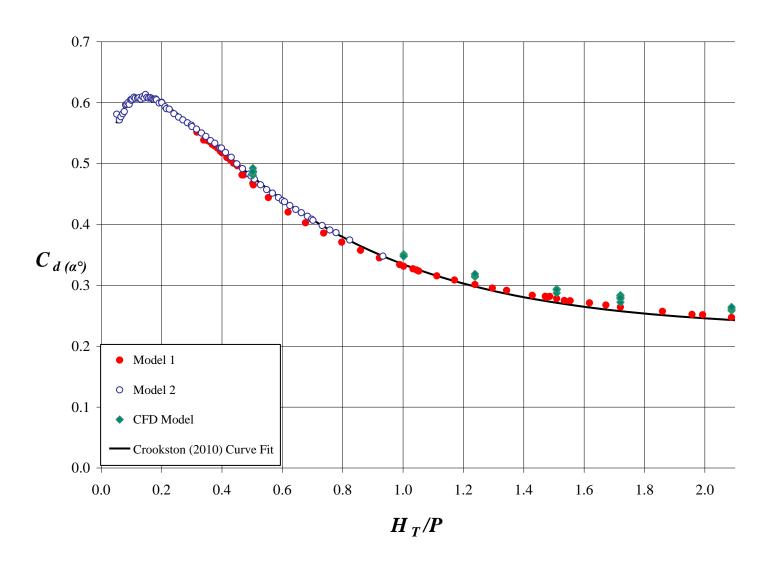
# Physical Modeling



## Numerical Modeling



## Results (15° Labyrinth)



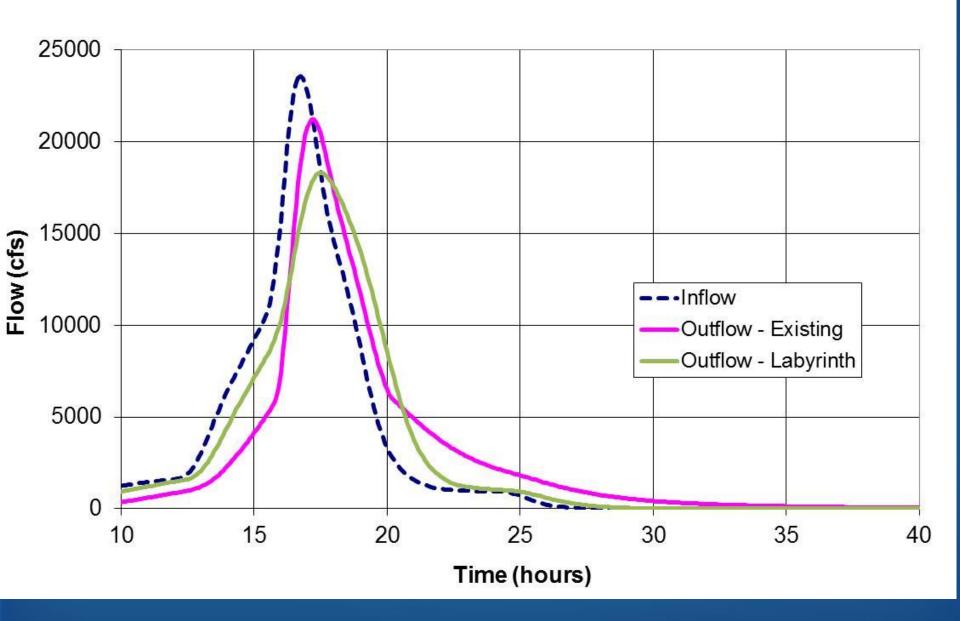
## Spillway Capacity

- Systems Approach
  - Passing the Peak
  - Flood Storage Reserve
  - Hydraulic Efficiency
- Spillway Replacement (Primary/Auxiliary)
- New Dams

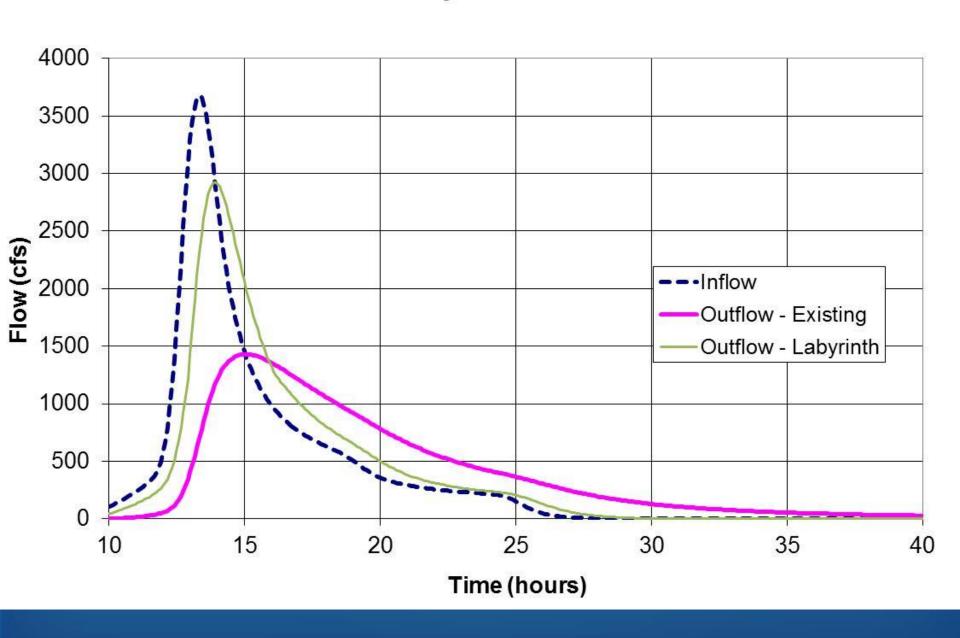








#### 100-year Flood



# Staged Weirs









### Gated Spillway Issues

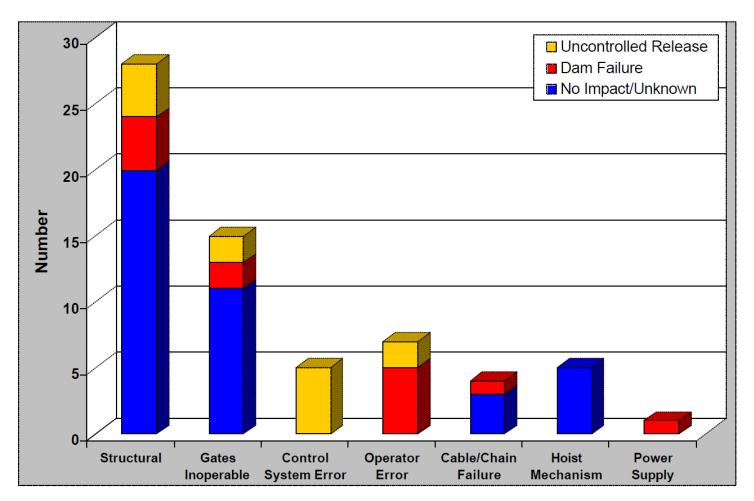
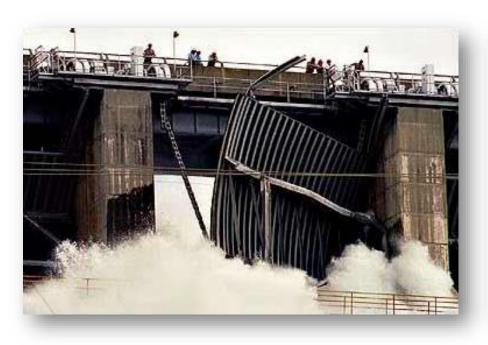


Figure 2 Dam gate system events and the consequences that resulted.

Source: *Performance of Hydraulic Systems*, National Performance of Dams Program, www.npdp.stanford.edu.

# Gated Spillways

• Dam and Gate Failures





# **Gated Spillways**

• Flooding...from gate operations?

## Flood Gates Opened at the J. Strom Thurmond Dam

Posted: Jul 11, 2013 6:14 PM EDT
Updated: Jul 11, 2013 6:35 PM EDT

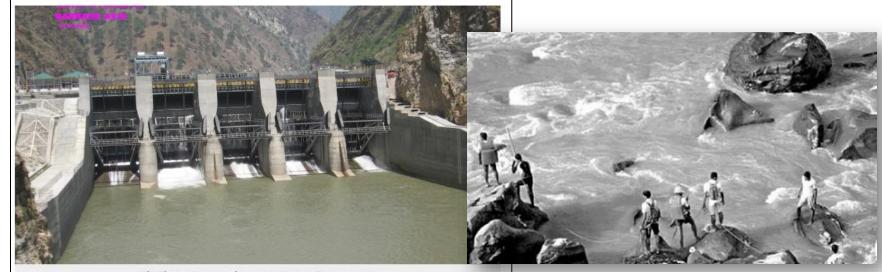
By Tyrone McCoy, WJBF Photojournalist

Connect

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## Larij Hydropower Project (2014)



File Photo: Largi Hydropower Project Downstream

#### 25 Hyd Students Feared Swept Away As Larji Dam Releases Water Without Notice

**Inquiry Report:** There are no standard operating procedures related to release of water...

The warning system is also inadequate. All this constitutes a systemic failure due to wrong and entrenched faulty procedure and practices...

### Tenughat Dam (2014)



Home

Sections

Subscription

#### 10 boys rescued after floodgates opened at Tenughat dam

Jun 21, 2014 12:36 PM, By PTI | o comments

Ten teenagers, who had gone fishing in Damodar river, were trapped for over eight hours when a sluice gate at the Tenughat dam was opened leading to sudden rise in water level, before they were rescued.

The boys escaped drowning by climbing atop a concrete platform built by the Chandrapura Thermal Power Station on Friday.

The incident at Pachaura village came close on the heels of the tragedy in Himachal Pradesh in which 24 engineering students from Hyderabad and a tour leader were washed away in the river when Larji hydropower project authorities suddenly released water from the barrage.

Bokaro Deputy Commissioner Uma Shankar Singh said, "The incident occurred when all the boys in the age group of 15/16 went to the river for fishing yesterday afternoon.

"As the water swelled following opening of one sluice gate at the Tenughat dam in Bokaro district, they climbed atop a concrete platform built by the Chandrapura Thermal Power Station yesterday."

The boys, who were residents of nearby villages, were rescued by police at around 11.30 p.m. on Friday, said.



#### In the US...









Residents call for new dam outflow schedule

Josh O'Leary, Iowa City Press-Citizen

11:20 p.m. CDT September 15, 2014

Residents on Monday questioned the U.S. Army Corps of Engineers' handling of July's flooding, while the corps defended itself against charges of both:

Not releasing enough water from the Coralville Reservoir before the flood.

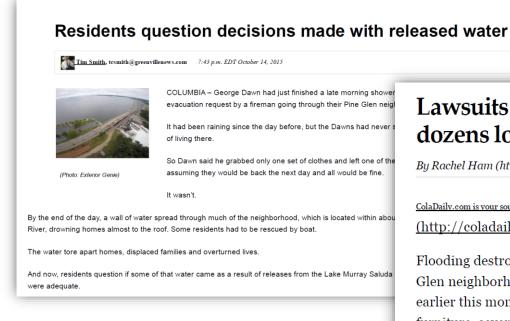
And later releasing too much water when there was dam capacity to spare.

Two months after Johnson County endured another summer flood, corps officials and representatives from local governments and the University of Iowa hosted a panel discussion at the Iowa City Public Library.

The discussion centered largely around the corps' management plan for the reservoir, which determines the schedule for when and how much water is released from the dam — a schedule that all seem to agree is due to be reevaluated. The plan was last revised more than a decade ago, but the corps'

better control it," Cathy Wilcox, a Taft Speedway resident, told the panelists

#### In the US...



"They gave us no warning." she said. "The "This all started because SCE&G decided to flood our neighborhood. They say it's not their fault, but they knew the rain was coming. They could have let the lake down before it hit." hydroelectric plant was releasing water...

#### Lawsuits mount against SCE&G after dozens lose homes during floods

By Rachel Ham (http://coladaily.com/author/rachel/) on October 27, 2015

ColaDaily.com is your source for free news and information in Columbia and the Midlands.

(http://coladaily.com)

Flooding destroyed numerous houses in the Coldstream and Pine Glen neighborhoods near Irmo during heavy rainfall and flooding earlier this month. After losing family mementos, pets and furniture, several families are filing lawsuits against SCE&G.

SCE&G announced Oct. 4 that officials would be opening the spillway gates to lower the levels in Lake Murray and alleviate pressure on the dam. A warning about "a significant increase in water flow in the lower Saluda River" was issued at that time.

Attorney Jake Moore said he is working about 50 lawsuits on behalf of clients after the Saluda River flooded their homes. Moore said he has no plans right now to create a class action suit.







#### Considerations in Labyrinth Spillway Design

- Siting & Sizing
- Head/Discharge Requirements
- Downstream flow conditions
- Existing spillway hydraulics

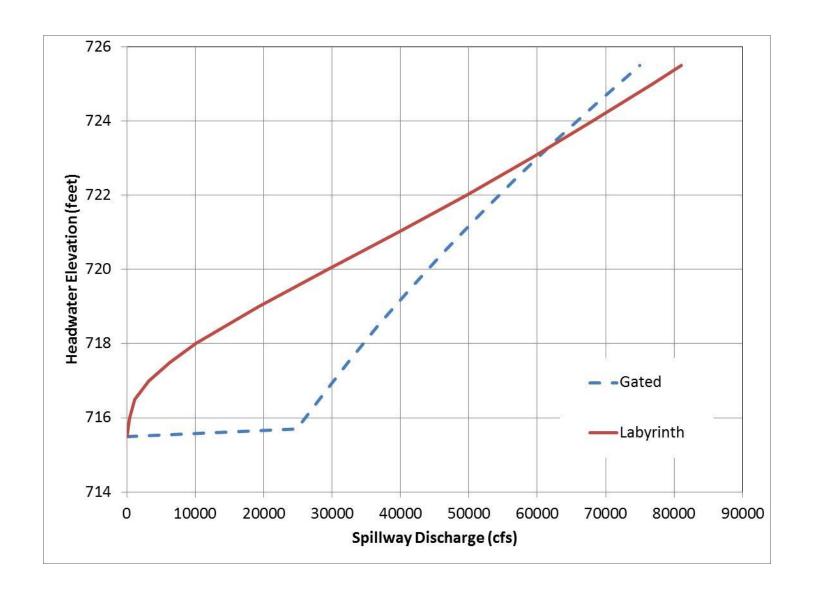




## Spillway Capacity Design

- Replace gated spillway with labyrinth weir with similar capacity (82,000 cfs)\* at top of dam (H=10 ft)
- Armor Embankment to safely pass SDF plus failures of upstream dams ( $Q_{in}$ =213,000 cfs)
- \* Assumes gates are fully operational

#### Gates vs. Fixed Crest



# Hydraulic Modeling



## Linville Land Harbor Dam



#### Linville Land Harbor Dam



#### Linville Land Harbor Dam



#### Linville Land Harbor Dam



#### A Tale of Two Spillways:

# The First Two Piano Key Weirs Constructed in the United States

J RYAN COLLINS SAMUEL KEES GERALD ROBBLEE RANDALL BASS

#### INTRODUCTION

Non-linear wetr structures can gready increase the discharge capacity as compared to linear wetrs within the same channel width. Labyrinth wetrs have been constructed in the United States for decades. Research of the hydraulic performance of labyrinth wetrs has been performed to better understand geometric effects of the wetrs on the discharge capacity. Some notable studies include "Wetrs with oblique and Zig-Zag Crests" (Gentlint, 1941). "Performance and Destgn of Labyrinth Weirs" (Hay and Taylor, 1970), "Discharge Characteristics of Labyrinth Weirs" (Liux, 1984), "Destgn of Labyrinth Spillways" (Tullis et al., 1995), and "Labyrinth Weirs" (Crookston, 2010), though there are many more.

A Piano Key Weir (PKW) is another variation of a non-linear weir, which has not been used before in the United States. The PKW has been used in France, Vietnam, Australia, and other parts of the world, but has not yet gained the same level of popularity in the United States. This article describes Schnabel Engineering's first PKW projects at two locations in the Southeastern United States (Peachtree City, Georgia, and Cedar Grove, North Carolina).

#### **ADVANTAGES OF PKWs**

PKW spillways provide unique hydraulic advantages, particularly when the available footprint dimensions are limited. The rectangular configuration of the "keys" provides a significant increase of weir length within a given channel width. The short base length and cantilevered apex geometry allow for even greater weir length within a relatively small footprint, making the use of PKWs convenient as a retrofit over an existing gravity section or where conventional labytinth weirs would otherwise not be feasible due to available base length limitations. Figure 1 (Paxson, Laugier 2014) depicts typical geometric parameters of both labytinth weirs and PKWs.

The PKW was introduced by Lempérière and Oumane in 2003 (Paxson, Laugher, 2014). The first known PKW installation was at the Goulours Dam in France in 2006 (Laugher, 2007). Since then, hydraulic engineers and researchers have continued to study the effects of the PKW geometry on the discharge capacity in an effort to optimize design parameters and better predict the head-discharge relationship of PKW spillways. Some of the impactful geometric ratios considered in the studies include the total hydraulic head to

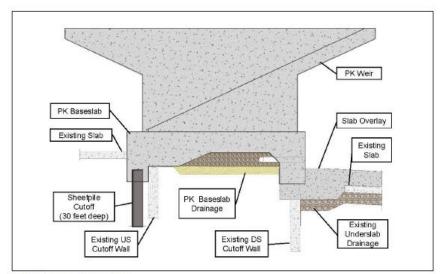


Figure 11: Proposed PK Weir Cross Section

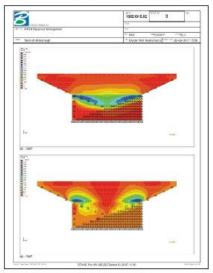


Figure 12: PK Divider Wall STAAD FE Model Output



Figure 13: WFER Construction Progress as of January 8, 2019

pashing the divider walls away from the inlet ramp). To reduce these deflections, adjacent divider walls are structurally connected at the inlet ramps with full horizontal reinforcement across the Joints. The detailing of the reinforcement included form savers at these connections to resist tension in the Joints between the inlet ramps and divider walls. Smooth dowels are included for the connection between the outlet ramps and divider walls as water contained in the inlet ramps would push the divider walls into the outlet ramps and the upstream Joints were in compression.

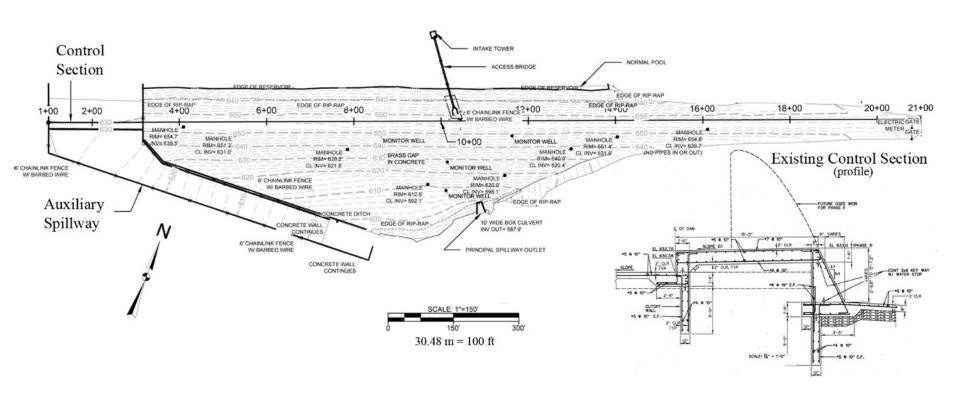
#### Piano Key Weirs in USA







#### Hillsborough -WFER

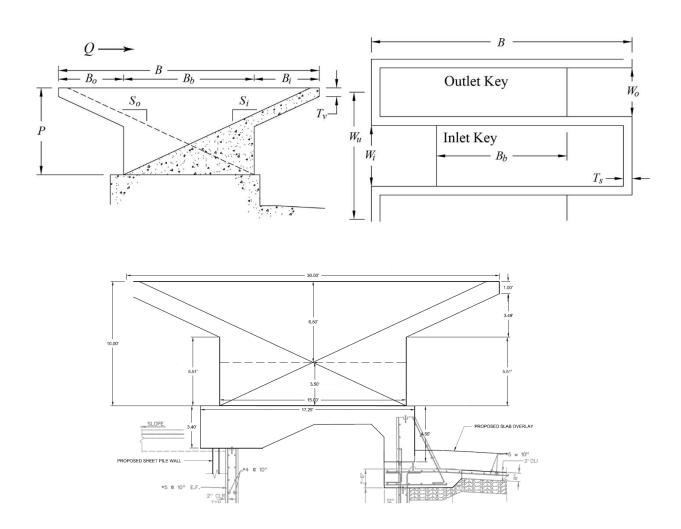


## Existing Auxiliary Spillway

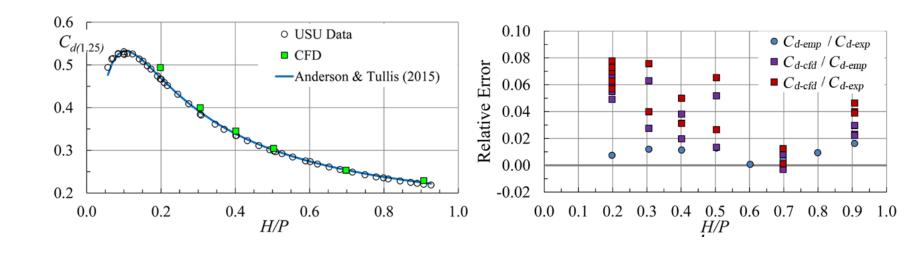


Spillway Alternative	Normal	100-year Storm		¾ PMP (SDF)	
	Pool EL (ft)	Peak Q (cfs)	Peak WS EL (ft)	Peak Q (cfs)	Peak WS EL (ft)
Existing	632.3	1,750	633.7	18,590	641.7
Proposed Ogee Weir	642.2	1,420	643.8	17,840	649.6
Proposed PK Weir	642.2	2,180	643.5	15,720	649.7

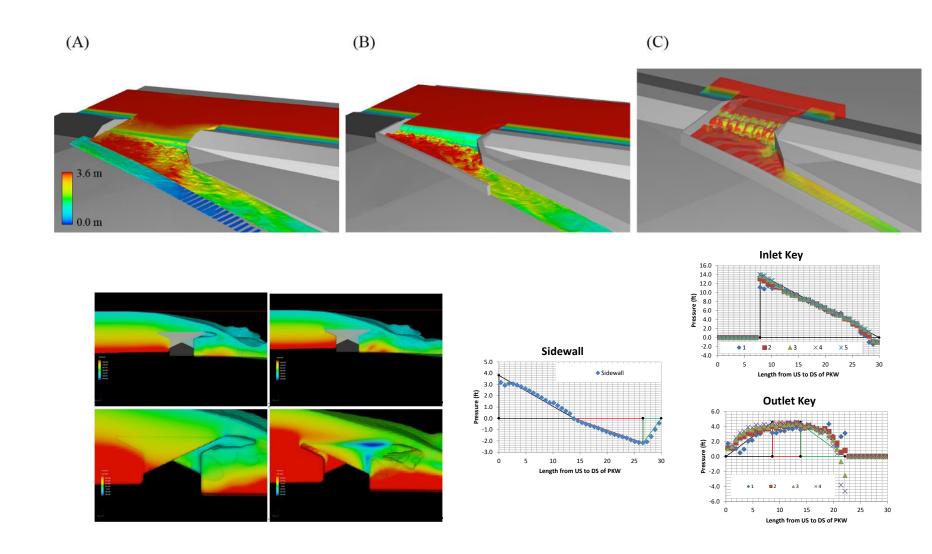
## Hillsborough - WFER



#### Hillsborough -WFER



## Hillsborough -WFER







#### Questions/Discussion



Pipestem Dam, North Dakota (model at US Bureau of Reclamation)



Lake Isabella Dam, California